

This Page Is Inserted by IFW Operations
and is not a part of the Official Record

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images may include (but are not limited to):

- BLACK BORDERS
- TEXT CUT OFF AT TOP, BOTTOM OR SIDES
- FADED TEXT
- ILLEGIBLE TEXT
- SKEWED/SLANTED IMAGES
- COLORED PHOTOS
- BLACK OR VERY BLACK AND WHITE DARK PHOTOS
- GRAY SCALE DOCUMENTS

IMAGES ARE BEST AVAILABLE COPY.

As rescanning documents *will not* correct images,
please do not report the images to the
Image Problem Mailbox.

(19)



Europäisches Patentamt
European Patent Office
Office européen des brevets



(11) Publication number:

0 321 662 B1

(12)

EUROPEAN PATENT SPECIFICATION(45) Date of publication of patent specification: **16.02.94** (51) Int. Cl.⁵: **G01L 3/10**(21) Application number: **88116294.5**(22) Date of filing: **01.10.88**(54) **Torque measuring device.**

(30) Priority: **28.12.87 JP 334861/87**
28.12.87 JP 334862/87
28.12.87 JP 334863/87
28.12.87 JP 334864/87

(43) Date of publication of application:
28.06.89 Bulletin 89/26

(45) Publication of the grant of the patent:
16.02.94 Bulletin 94/07

(84) Designated Contracting States:
DE ES FR GB IT SE

(56) References cited:
EP-A- 0 136 086 DE-A- 3 206 503
DE-A- 3 511 442 DE-A- 3 704 049
FR-A- 2 032 215 FR-A- 2 564 585
US-A- 2 553 833

Patent Abstracts of Japan, vol. 12, no. 66
(P-671)(2913), February 27, 1988 & JP-A-62
206 421

Patent Abstracts of Japan, vol. 9, no. 221
(P-386)(1944), September 7, 1985 & JP-A-60
79 240

(73) Proprietor: **KUBOTA, LTD**
2-47, Shikitsuhigashi 1-chome
Naniwa-ku
Osakashi Osaka 556(JP)

(72) Inventor: **Takada, Shiro Hirakata Plant of**
Kubota, Ltd.
1-1, Nakamiya Oike 1-Chome
Hirakata-Shi Osaka(JP)
 Inventor: **Kimura, Hitoshi Kyuhoji Plant of**
Kubota, Ltd.
2-35, Jinmu-Cho
Yao-Shi Osaka(JP)
 Inventor: **Ishino, Renshiro Hirakata Plant of**
Kubota, Ltd.
1-1, Nakamiya Oike 1-Chome
Hirakata-Shi Osaka(JP)
 Inventor: **Yoshimura, Shigeo Hirakata Plant of**
Kubota, Ltd.
1-1, Nakamiya Oike 1-Chome
Hirakata-Shi Osaka(JP)

(74) Representative: **Meyer, Ludgerus A., Dipl.-Ing.**
et al
Patentanwalt
Jungfernstieg 38
D-20354 Hamburg (DE)

Note: Within nine months from the publication of the mention of the grant of the European patent, any person may give notice to the European Patent Office of opposition to the European patent granted. Notice of opposition shall be filed in a written reasoned statement. It shall not be deemed to have been filed until the opposition fee has been paid (Art. 99(1) European patent convention).

Description

FIELD OF THE INVENTION

The present invention relates to a torque measuring device and particularly to a torque measuring device capable of non-contact measurement of torque in the shafts of engines, motors, industrial machines and the like.

BACKGROUND OF THE INVENTION

This type of torque measuring device is disclosed in Japanese Patent No. 169326. In this device, a shaft having soft magnetic and magnetostrictive properties is formed on its outer periphery with a pair of knurled regions inclined in opposite directions to form angles of 45 degrees with respect to the axis of rotation of the shaft, each knurled region having an exciting coil and a detecting coil wound along the outer periphery thereof.

According to such arrangement, the knurled regions provide magnetic anisotropy, and a change in permeability occurring in each knurled region according to transmission torque is detected by the detecting coil. At this time, when a compressive force acts on one of the knurled region in the knurling direction, a tensile force acts on the other knurled region since the knurled regions are inclined in opposite directions. As a result, the detection voltage on one of the detecting coils increases with increasing torque while the detection voltage on the other detecting coil decreases. If the detection voltages on these detecting coils are, subtracted one from the other a torque detection voltage indicating a change in torque can be obtained.

Another conventional torque detecting device is disclosed in Japanese Patent Application Laid-Open Specification No. 59-166827. In this device, instead of forming the knurled regions shown in aforesaid Japanese Patent No. 169326, amorphous soft magnetic layers inclined in opposite directions are formed on the surface of a rotary shaft by bonding, plating or the like. According to such an arrangement, measurement of torque is also possible on a shaft having no magnetostrictive property.

With these conventional arrangements, however, the balance of detection voltages outputted from the two detecting coils with no transmission torque being imposed tends to change owing to temperature changes and time-dependent changes. This is due to changes in magnetic properties (permeability and magnetostriction factor) of the material of the shaft and changes in iron loss caused by magnetic lines passing through the shaft surface and variations in the quality of exciting coils, detecting coils and magnetic layers on the

shaft according to material and manufacture. As a result, the sensitivity, the zero point (output value when the torque is zero) and the like changes, causing error in measured torque values. Patent Abstracts of Japan, vol. 12, No. 66 (P-671)(2913), 27/02/88; Pub. No. 62-206421 describes a device for measuring torque applied on a nonmagnetic shaft using a pair of detecting coils (C1,C2) and a pair of correcting coils (C3,C4).

DISCLOSURE OF THE INVENTION

With the above in mind, an object of the invention is to prevent errors from being produced in measured torque values owing to changes in the balance, zero point and sensitivity.

To achieve this object, the present invention is directed to an arrangement comprising:

torque detecting means having first and second torque detecting magnetically anisotropic regions formed on the outer peripheral surface of a torque transmitting shaft and provided with magnetic anisotropy such that the regions are inclined in opposite directions to form angles with respect to the axis of rotation of said shaft, and first and second detecting coils capable of detection changes in permeability in the torque detecting magnetically anisotropic regions,

exciting coils provided for respective detecting coils and correcting coils, and

correcting means having first and second correcting magnetically anisotropic regions, with magnetic anisotropy imparted thereto in a direction parallel with the axis of rotation of said shaft, formed on the outer peripheral surface of said shaft in the vicinity of said first and second torque detecting magnetically anisotropic regions, and first and second correcting coils capable of detecting changes in permeability in the correcting magnetically anisotropic regions.

According to such arrangement, the correcting magnetically anisotropic regions have magnetic anisotropy imparted thereto in a direction parallel with the axis of rotation of the shaft, and the outputs from the correcting coils are hardly influenced by the torque in the shaft; thus, only those outputs which are related to permeability and magnetostriction factor can be delivered. Since such correcting magnetically anisotropic regions and correcting coils are installed in the vicinity of the torque detecting magnetically anisotropic regions and detecting coils, respectively, different errors can be separated from the torque detection data and then corrected.

A second aspect of the invention is directed to an arrangement comprising:

torque detecting means having first and second torque detecting magnetically anisotropic re-

gions formed on the outer peripheral surface of a torque transmitting shaft and provided with magnetic anisotropy such that the regions are inclined in opposite directions to form angles with respect to the axis of rotation of said shaft, and first and second detecting coils capable of detecting changes in permeability in the torque detecting magnetically anisotropic regions, and exciting coils provided for respective detecting coils and correcting coils, and

correcting means having a correcting shaft separate from said torque transmitting shaft and free from load, and first and second correcting coils, installed around the correcting shaft,

wherein said correcting means having substantially the same magnetic properties as said torque detecting means and installed in the vicinity of said torque detecting means.

According to such arrangement, the correcting shaft is never loaded since it is separated from the torque transmitting shaft. Therefore, by detecting the outputs from the two correcting coils and controlling an exciting AC source so as to make their detection voltage constant, the various errors occurring at the time of torque detection and caused by temperature changes and time-dependent changes can be corrected while being hardly influenced by torque signal.

A third aspect of the invention is directed to an arrangement comprising:

a torque detecting magnetically anisotropic region provided with magnetic anisotropy such that the region is inclined to form an angle with respect to the axis of rotation of a torque transmitting shaft,

a correcting magnetically anisotropic region formed on the outer peripheral surface of the shaft in the vicinity of the torque detecting magnetically anisotropic region and provided with magnetic anisotropy in a direction parallel with the axis of rotation of the shaft,

a detecting coil and a correcting coil installed along said torque detecting magnetically anisotropic region and said correcting magnetically anisotropic region, respectively, including a detection-purpose exciting coil associated with the detecting coil and a correction-purpose exciting coil associated with the correcting coil, and

means for controlling the exciting voltage applied to said exciting coil of the correcting coil to ensure that the measured data provided by said correcting coil is equal to a certain reference value and for controlling the exciting voltage applied to said exciting coil for said detecting coil correspondingly to the control of said exciting voltage of the exciting coil of the correcting coil.

According to such arrangement, since the exciting voltage for the correcting coil is controlled so that the measured data is equal to a certain refer-

ence value and since the exciting voltage for the detecting coil is controlled in conjunction therewith, the detection sensitivity is kept at a constant level. As a result, the gradient of the detection voltage and the output level under constant torque load are kept constant; thus, the torque detecting sensitivity is prevented from changing. In this case, since the correcting magnetically anisotropic region is formed to extend parallel with the axis of the shaft, the output from the correcting coil is not influenced by the torque acting on the shaft. Therefore, the measured data provided by the correcting coil is controlled to a constant value irrespective of the presence and amount of the torque load on the shaft and time-dependent changes and temperature changes in the magnetic properties of the shaft; thus, the detecting coil sensitivity is maintained at a constant level.

A fourth aspect of the invention has been made object of a divisional application.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic view of a torque measuring device according to a first embodiment of the invention;

Fig. 2 is a block diagram showing the torque measuring device of Fig. 1 together with an electronic circuit for torque measurement;

Fig. 3 is a graph showing detected voltages from detecting coils when there is no error;

Fig. 4 is a graph showing a torque signal based on Fig. 3;

Fig. 5 is a graph showing detected voltages when the balance between the torque detecting regions is upset;

Fig. 6 is a graph showing a torque signal based on Fig. 5;

Fig. 7 is a graph showing detected voltages obtained with a predetermined sensitivity;

Fig. 8 is a graph showing detected voltages when the sensitivity changes;

Fig. 9 is an operation timing chart for the circuit shown in Fig. 2;

Fig. 10 is a diagram showing the arrangement of a torque measuring device according to a second embodiment of the invention;

Fig. 11 is a view showing the principal portion of the shaft shown in Fig. 10 and periphery thereof;

Fig. 12 is a view showing the arrangement of a torque measuring device according to a modification of the second embodiment of the invention;

Fig. 13 is a view showing a torque measuring device according to a third embodiment of the invention;

Fig. 14 is a view showing the principal portion of the shaft shown in Fig. 13 and periphery thereof;

Fig. 15 is a graph showing, by way of example, detected voltages obtained by the device shown in Fig. 13; and

Fig. 16 is an operation timing chart for the device of Fig. 13.

DESCRIPTION OF THE EMBODIMENTS

FIRST EMBODIMENT

In Fig. 1, the numeral 11 denotes a torque transmitting the output of an engine to a working apparatus. The outer peripheral surface of the shaft 11 is formed with torque transmitting magnetically anisotropic regions 12 and 13 provided with magnetic anisotropy such that it is inclined in opposite directions to form angles of 20-60 degrees, preferably 45 degrees with respect to the axis of rotation of the shaft 11, and axially spaced a predetermined distance from each other. These detecting magnetically anisotropic regions 12 and 13, as described above, can be formed by knurling the outer peripheral surface of the shaft 11 or by forming amorphous ferromagnetic layers on the surface of the shaft 11 by bonding, plating or other method.

At positions axially spaced from each other and across said torque detecting magnetically anisotropic regions 12 and 13, there are provided correcting magnetically anisotropic regions 14 and 15 formed on the outer peripheral surface of the shaft 11 in the vicinity of said torque detecting magnetically anisotropic regions 12 and 13. These correcting magnetically anisotropic regions 14 and 15 are provided with magnetic anisotropy in a direction parallel with the axis of rotation of the shaft 11 and are created by the axial magnetic anisotropy formation using the same process, such as knurling or amorphous layer formation, as in the torque detecting magnetically anisotropic regions 12 and 13.

Exciting coils 16, 17, 18 and 19 are positioned around the outer peripheries of the magnetically anisotropic regions 12, 13, 14 and 15. Disposed on the respective outer sides of the exciting coils 16, 17, 18 and 19 are detecting coils 20 and 21 associated with the torque detecting magnetically anisotropic regions 12 and 13 and correcting coils 22 and 23 associated with the correcting magnetically anisotropic regions 14 and 15. The numeral 24 denotes a core made of a ferromagnetic material such as silicon steel sheet or ferrite and defining a passage for magnetic flux and also serving as a casing for accommodating the coils 16 through 23.

Fig. 2 shows a torque measuring circuit. In this figure, the numeral 25 denotes an oscillator connected to a first AC power source 26 in the form of a power amplifier. Connected to the output terminal of the oscillator 25 in parallel with the first power

source 26 is the input terminal of a second power source 27 also in the form of a power amplifier. The exciting coils 16 and 18 are combined in series and connected to the second power source 27, while the exciting coils 17 and 19, also connected in series, are connected to the first power source 26. The detecting coils 20 and 21 and the correcting coils 22 and 23 are connected to a CPU 40 respectively through rectifiers 29, 30, 28 and 31, filters 33, 34, 32 and 35 each formed of a resistor and a capacitor, and AD converters 37, 38, 36 and 39.

A power source cut-off signal line 41 for cutting off the outputs of the two power sources 26 and 27 is connected, together with an DA converter 42, to the CPU 40. Also connected to the CPU 40 are power source controlling signal lines 43 and 44 for adjusting the amplification factors of the power amplifiers constituting the two power sources 26 and 27 to control their outputs. The numerals 45 and 46 denote DA converters placed in the signal lines 43 and 44. The numeral 47 denotes a reference value setting device adapted to transfer a reference value E_s digitally set or software-wise set to the CPU 40. Further, the CPU 40 has a timing circuit 48 connected thereto to set the operation timing for the present circuit. The numeral 49 denotes an output terminal of a torque signal. The numerals 50, 51 and 52 denote manual switches used to correct various errors, as will be later described, irrespectively of the operation timing for the present circuit.

The operation based on the above arrangement will now be described. When the power sources 26 and 27 are turned on, output voltages appear in the detecting coils 20 and 21 and the correcting coils 22 and 23, said voltages taking values V_1 , V_2 , S_1 , and S_2 on the output side of the AD converters 37, 38, 36 and 39, i.e., the input side of the CPU 40. Further, these values are arithmetically processed in the CPU 40 to be converted into values V_1' , V_2' , S_1' and S_2' .

When a torque acts on the shaft 11, the output voltages from the detecting coils 20 and 21, after passing through the AD converters, are V_1 and V_2 , shown in Fig. 3. These values V_1 and V_2 are processed in the CPU 40, as will be later described, and thereby converted into values V_1' and V_2' . The difference $(V_1' - V_2')$ is multiplied by a suitable value k , and the value $k(V_1' - V_2')$ is outputted as a torque signal from the output terminal 49. Fig. 4 shows an example of a torque signal T based on the outputs V_1 and V_2 of Fig. 3.

Errors due to temperature changes and time-dependent changes are corrected as follows.

First, the zero point adjustment is made. To this end, the outputs from the two power sources 26 and 27 are cut off with predetermined timing, for

example, once in every 1 minute, through the power source cut-off signal line 41. Then, since the exciting voltages for the exciting coils 16, 17, 18 and 19 become zero, the output voltages from the detecting coils 20 and 21 and the correcting coils 22 and 23 become also zero. Therefore, if the outputs from the AD converters 37, 38, 36 and 39 have values other than zero, for example, $V_1 = \epsilon_1$, $V_2 = \epsilon_2$, $S_1 = \delta_1$ and $S_2 = \delta_2$, then these errors are due to some causes, such as temperature drift in the electronic circuit. Thus, calibration is made by the CPU 40 through arithmetic operation so that $V_1' = V_1 - \epsilon_1$, $V_2' = V_2 - \epsilon_2$, $S_1' = S_1 - \delta_1$ and $S_2' = S_2 - \delta_2$. When the arithmetic operation for the zero point correction is completed, $V_1' = V_2' = S_1' = S_2' = 0$. And with the timing which follows the completion of the zero point adjustment, new data V_1' , V_2' , S_1' and S_2' with the circuit errors ϵ_1 , ϵ_2 , δ_1 and δ_2 corrected are obtained.

With the next timing, the balance correction of the two detecting sections and the two correcting sections is made. The balance between the detecting coils 20 and 21 can be upset as the magnetic properties of the shaft are influenced by temperature changes or by long-term alternate torque or as the temperature in the interior of the torque measuring device changes. When the balance between the detecting coils 20 and 21 is upset, the detected voltages V_1 and V_2 are as shown in Fig. 5, and the torque signal T corresponding thereto changes from the normal state, as shown in Fig. 6; thus, this is corrected.

The difference $S_1' - S_2'$ between the calibrated data S_1' and S_2' of the corrected voltages S_1 and S_2 is calculated in the CPU 40. And a control signal is fed to the second power source 27 through the power source control signal line 43 and the power source 27 is controlled so that $S_1' - S_2' = 0$. Thereby, the exciting voltages for the series-connected exciting coils 16 and 18 are simultaneously adjusted, the outputs S_1 and V_1 are corrected, and the balance between S_1 and S_2 , that is, the balance between V_1 and V_2 is simultaneously corrected. As a result, the diagrams shown in Figs. 3 and 4 are corrected so that a state close to $V_1 = V_2$ is established at torque zero state.

Next, sensitivity correction is made. At the aforesaid stage where said balance correction is made, the crossing point A between the output lines for the two signals V_1' and V_2' lies on the zero-torque line, as shown in Fig. 7. However, if the magnetic properties of the shaft change owing to temperature changes, the gradients of the output lines for the two signals V_1' and V_2' (that is, sensitivity) change and so does the average level E_m in Fig. 7, with E_m changing to E_m' as shown in Fig. 8. As a result, the inclination of the torque signal line indicated by $k(V_1' - V_2')$ (see Fig. 4) changes

and so does the measurement sensitivity.

Thus, correction is effected to bring E_m' back to the predetermined value E_m and restore the predetermined inclination to ensure that the sensitivity characteristic is constant.

The sum of the two signals $V_1' + V_2'$ (which is twice the average value), is used as a detected value representing the average value. Control is effected to ensure that this value is equal to the set value E_s inputted into the CPU 40 by the reference value setting device 47, that is, $\frac{1}{2}(V_1' + V_2') - E_s = 0$. Concretely, the first and second power sources 26 and 27 are adjusted by the power source control signal line 44 so as to increase or decrease their output levels. Then the two power sources 26 and 27 simultaneously increase or decrease in output level, and control is effected to ensure that $\frac{1}{2}(V_1' + V_2')$ is equal to E_s without upsetting the balance between the two detecting sections. When the output levels of the two signals V_1' and V_2' are restored to the predetermined values in this manner, their angles of inclination are also restored to the predetermined values, as shown in broken lines in Fig. 8; thus, the sensitivity correction is completed.

The aforesaid zero point correction, balance correction and sensitivity correction are effected in this order with predetermined timing by the timing circuit 48. For example, with 1 cycle assumed to be 1 minute, the zero point correction is made in the first 50 milliseconds, followed by the balance correction in the next 50 milliseconds, and the sensitivity correction is made at all times, that is, many times in the remaining time. Such cycle is performed repeatedly. During the zero point correction and balance correction, the torque signal at the end of the time of the preceding cycle is outputted from the terminal 49.

In addition to such automatic cyclic operation, manual correction can be made on demand.

For example, if the manual switch 50 for zero point correction is operated, the signal therefrom is taken into the CPU 40 and during the time this switch is being operated, the aforesaid zero point correcting operation is repeatedly performed. At this time, it is possible to inform the operator by a suitable method that the correcting operation is going on. When the switch operation is completed, the measured torque value $k(V_1' - V_2')$ according to the data after correction is outputted.

When the manual switch 51 for balance correction is pressed, the aforesaid balance correcting operation is performed. Such manual operation is performed in the event that although there is no torque load, the balance in the detection state on both sides is upset so that the torque indication does not become 0, as shown in Fig. 6.

When the manual switch 52 for sensitivity correction is used for manual correction, for example, upon completion of manufacture of the present device, the rated reference torque is applied to the shaft 11 as by a lever and a weight and the reference value setting device 47 is adjusted so that the indicated value coincides with the rated value.

As described above, according to the present device, the temperature change, time-dependent change and zero point change of the torque output signal can all be automatically corrected. Particularly, the sensitivity change and zero point change due to temperature change during torque loading can be automatically corrected. Further, the electronically processing circuit is very simple in that only the CPU 40 exists except for the AD converters 36, 37, 38 and 39 and the DA converters 42, 45 and 46. This is due to the fact that the automatic correction of various errors is made by software.

Though not described in the above for the sake of simplicity, the zero point correction at the time of manufacture of the device is made in addition to the zero point correction associated with temperature changes and time-dependent changes. This is made by operating the manual zero correction switch 50 with torque load on the shaft 11 removed, that is, with no torque when the first adjustment of the present device is made, and storing a torque indication value B_0 from the torque output terminal 49 due to unbalance between the two detecting sections in a non-volatile memory in the CPU 40. And thereafter, actually, the torque indication value

$$k = (V_1' - V_2') - B_0$$

appears at the terminal 49.

SECOND EMBODIMENT

In Fig. 11, the outer peripheral surface of a torque transmitting shaft 11 is provided with a pair of inclined, torque detecting magnetically anisotropic regions 12 and 13 alone unlike the first embodiment.

In the vicinity of the shaft 11, a correcting shaft 55 free from torque is provided in a location where it is subjected to substantially the same environmental conditions including temperature. The outer peripheral surface of this correcting shaft 55 is provided with correcting magnetically anisotropic regions 56 and 57 inclined in opposite directions at an angle of 20-60 degrees, preferably 45 degrees with respect to the axis of the shaft 55, as in the case of the torque detecting magnetically anisotropic regions 12 and 13 on the shaft 11.

The magnetically anisotropic regions 12, 13, 56 and 57 have exciting coils 16, 17, 18 and 19 disposed around their respective outer peripheries. Further, disposed around the respective outer peripheries of the exciting coils 16, 17, 18 and 19 are detecting coils 20 and 21 associated with the torque detecting magnetically anisotropic regions 12 and 13 and correcting coils 22 and 23 associated with the correcting magnetically anisotropic regions 56 and 57. The numerals 24 and 54 denote cores made of soft magnetic material and providing a passage for the magnetic flux and utilized as a casing for accommodating the coils. The torque detecting section around the shaft 11 and the correcting section around the shaft 55 are manufactured so that they have substantially the same magnetic properties as by providing the magnetically anisotropic regions with the same characteristics.

Fig. 10 shows the entire arrangement of the present device including an electronic circuit. In this figure, the same members as those shown in Fig. 2 are indicated by the same reference numerals. In this case, however, the exciting coils 16 and 18 are combined in series and connected to a first power source 26, while the exciting coils 19 and 17 are also combined in series and connected to a second power source 27.

According to this arrangement, as in the case of the first embodiment, zero point correction, balance correction and sensitivity correction are made with the timing shown in Fig. 9. The details of these corrections are omitted as they are the same as in the first embodiment. The device is also the same in that manual switches 50, 51 and 52 are provided for making said corrections on demand. In this embodiment also, the torque indication value appearing at the torque output terminal 49 is shown in a simplified manner in Fig. 10.

Fig. 12 shows a device having a modified shaft 55. In this modified example, the shaft 55 has no magnetically anisotropic region formed thereon. Even if the magnetically anisotropic region is omitted, there will be no trouble in practice unless the coincidence between the magnetic properties of the torque detecting section around the shaft 11 and the correcting section around the shaft 55 is degraded. In other words, if changes in the magnetic properties corresponding to temperature changes are substantially the same for both shafts 11 and 55, then the omission of formation of magnetically anisotropic region on the shaft 55 is allowed.

Though not shown, a magnetically anisotropic region which extends parallel with the axis of the shaft 55 may be formed on the shaft 55, as in the case of the correcting magnetically anisotropic regions 14 and 15 shown in Fig. 1.

THIRD EMBODIMENT

In Fig. 14, the outer peripheral surface of a shaft 11 is provided with a torque detecting magnetically anisotropic region 12 forming an angle with respect to the axis of the shaft 11, and a correcting magnetically anisotropic region 14 which is located in the vicinity of said detecting magnetically anisotropic region 12 and extending parallel with the axis. Exciting coils 16 and 17 are disposed around the magnetically anisotropic regions 12 and 14. Further, disposed around the outer peripheries of the exciting coils 16 and 17 are a detecting coil 20 corresponding to the torque detecting magnetically anisotropic region 12 and a correcting coil 22 corresponding to the correcting magnetically anisotropic region 14. The numeral 24 denotes a core.

Fig. 13 shows the entire arrangement of the present device including an electronic circuit. In this figure, the numeral 25 denotes an oscillator, and 26 denotes an AC power source. The exciting coils 16 and 17 are combined in series and connected to the power source 26. The detecting coil 20 and correcting coil 22 are connected to the CPU 40 respectively through rectifiers 29 and 28, filters 33 and 32, and AD converters 37 and 36. A power source cut-off signal line 41 for cutting off the output of the power source 26 is connected to the CPU 40 together with an DA converter 42. Further, a power source control signal line 44 for controlling the output of the power source 26 is connected to the CPU 40 through a DA converter 42. The numeral 48 denotes a timing circuit; 49 denotes an output terminal for torque signals; and 50 and 52 denote manual switches.

The operation based on the above arrangement will now be described. When the power is turned on, output voltages appear at the detecting coil 20 and correcting coil 22, said voltages having values V and S at the respective output sides of the AD converters 37 and 36, i.e., at the input side of the CPU 40.

With respect to these values V and S, as in the case of the first through third embodiments, with the output of the power source 26 turned off, zero point correction is made and these values are arithmetically processed to provide values V' and S'.

In this condition, however, the indication value $k(V' - S')$ obtained after re-throwing (returning) the power source 26 does not necessarily indicate zero, even if there is no torque. The reason is that the detecting and correcting sections are not necessarily magnetically balanced. Thus, when it is known that there is no torque (as when the present device is adjusted for the first time or the shaft 11 is not being driven), the manual switch 50 for

manual zero point adjustment is operated. Thereupon, a signal from the switch 50 is taken into the CPU 40, where the torque indication value B at the terminal 49 is subtracted from said indication value $k(V' - S')$ to make the output from the terminal 49 zero. This value B is stored in the CPU 40 until the next manual correction is made. Thereafter, the value $k(V' - S') - B$ is used as the indication value. Such processing corresponds to the "balance correction" in the first and second embodiments in that the operation is manual.

Next, sensitivity correction is made. If the characteristics of the device change owing to temperature changes or the like, the signals V' and S' vertically displace as indicated by two-dot-and-dash lines in Fig. 15 (the zero point correction value B being omitted), and the gradient of the calibrated value V' based on the signal from the detecting coil 20 also changes. As a result, the angle of inclination of the torque signal T indicated by $k(V' - S')$ changes.

Thus, by increasing or decreasing the level of the output from the power source 26 by the power source control signal line 44 while simultaneously increasing or decreasing the exciting voltages for the exciting coils 16 and 17, control is effected so that the calibrated value S' based on the signal from the correcting coil 22 is equal to the set value Es inputted into the CPU 40 by the reference value setting device 47, that is, so that $S' - E_s = 0$. Thereby, the values V' and S' shown in two-dot-and-dash lines in Fig. 15 are corrected to the values shown in solid lines, with the gradient of the calibrated value V' restored to the predetermined state; thus, the torque measuring sensitivity is corrected.

Since the correcting magnetically anisotropic region 14 is formed to extend parallel with the axis of the shaft 11, the calibrated value S' based on the output of the correcting coil 22 is constant as shown in Fig. 15 irrespectively of the amount of the torque. Therefore, the torque measuring sensitivity can be corrected irrespectively of the presence or absence and the amount of the torque.

Fig. 16 shows an operation timing for the circuit shown in Fig. 13, said timing being similar to the one shown in Fig. 9. However, only the zero point correction and sensitivity correction are automatically made by the CPU 40, as described above.

In the case where manual correction is to be made by using the manual switch 52 for sensitivity correction, this can be made by applying the rated torque to the shaft 11 by a lever and a weight and adjusting the reference value setting device 47 so that the prevailing indication value is equal to the rated value.

Then electronic circuit described in the preceding embodiments may be used with some of the functions of said circuit omitted. For example, only the circuit for controlling the zero point, the circuit for controlling the sensitivity or the circuit for controlling the balance may be utilized. These circuits are suitable where it is desired to control only changes in the zero point with high accuracy, where it is desired to control the sensitivity with high accuracy though allowing coarse control of the zero point, or in other cases. Such arrangement is advantageous in that the control circuit and control process can be simplified. An analogue electronic circuit which does not contain CPU can also be utilized.

Claims

1. A device for measuring torque acting on a shaft, comprising:
 - torque detecting means having first and second torque detecting magnetically anisotropic regions (12, 13) formed on the outer peripheral surface of a torque transmitting shaft (11) and provided with magnetic anisotropy such that the regions (12, 13) are inclined in opposite directions to form angles with respect to the axis of rotation of said shaft (11), and first and second detecting coils (20, 21) capable of detecting changes in permeability in the torque detecting magnetically anisotropic regions (12, 13), and
 - exciting coils (16, 17, 18, 19) provided for respective detecting coils (20, 21) and correcting coils (22, 23), and
 - correcting means having first and second correcting magnetically anisotropic regions (14, 15), with magnetic anisotropy imparted thereto in a direction parallel with the axis of rotation of said shaft (11), formed on the outer peripheral surface of said shaft in the vicinity of said first and second torque detecting magnetically anisotropic regions (12, 13), and first and second correcting coils (22, 23) capable of detecting changes in permeability in the correcting magnetically anisotropic regions (14, 15).
2. A device as set forth in claim 1,
 - wherein the exciting coil (16) for the first detecting coil (20) and the exciting coil (18) for the first correcting coil (22) being combined in series and connected to a first AC power source (27) and
 - wherein the exciting coil (17) for the second detecting coil (21) and the exciting coil (19) for the second correcting coil (23) being combined in series and connected to a second AC power source (26).
3. A device as set forth in Claim 2, including:
 - means (41, 42) for cutting off the outputs of the first and second power sources with suitable timing during torque measurement,
 - means for finding measured values provided by the first and second detecting coils (20, 21) and first and second correcting coils (22, 23) when said power sources are cut off, and
 - means for calibrating measured data by subtracting the readings in the two detecting coils and two correcting coils when said AC power sources are cut off from the measured values provided by said coils when the cut-off of said AC power sources is cancelled.
4. A device as set forth in Claim 3, including means for controlling one of the AC power sources so that calibrated values of the measured data provided by the two correcting coils (22, 23) are equal.
5. A device as set forth in Claim 4, including means for controlling the two AC power sources so that the sum of the calibrated values of the measured data provided by the two detecting coils (20, 21) is a constant reference value.
6. A device as set forth in Claim 5, including means which, with constant timing, allows one of the following processes to be executed or two or more thereof to be serially executed:
 - the process for calibrating the measured data provided by the two detecting coils (20, 21) and two correcting coils (22, 23),
 - the process for controlling one of the power sources (26, 27) so that the calibrated values of the measured data provided by the two correcting coils are equal, and
 - the process for controlling both of the power sources (26, 27) simultaneously so that the sum of the calibrated values of the measured data provided by the two detecting coils (20, 21) is a constant reference value.
7. A device as set forth in Claim 6, including means (50, 51, 52) which makes it possible to execute at least one of said three processes to be executed manually at any time irrespective of the constant timing.
8. A device for measuring torque acting on a shaft, comprising:
 - torque detecting means having first and second torque detecting magnetically anisotropic regions (12, 13) formed on the outer peripheral surface of a torque transmitting shaft (11) and provided with magnetic anisotropy such that the regions (12, 13) are

inclined in opposite directions to form angles with respect to the axis of rotation of said shaft (11), and first and second detecting coils (20, 21) capable of detecting changes in permeability in the torque detecting magnetically anisotropic regions (12, 13), and

exciting coils (16, 17, 18, 19) provided for respective detecting coils (20, 21) and correcting coils (22, 23), and

correcting means having a correcting shaft separate from said torque transmitting shaft (11) and free from load, and first and second correcting coils (22, 23) installed around the correcting shaft,

wherein said correcting means having substantially the same magnetic properties as said torque detecting means and installed in the vicinity of said torque detecting means.

9. A device as set forth in Claim 8, wherein:
the correcting shaft has first and second correcting magnetically anisotropic regions (56, 57) on the outer peripheral surface thereof which are inclined in opposite directions to form angles with respect to the axis of said correcting shaft, and
the first and second correcting coils (22, 23) are installed along the periphery of said first and second magnetically anisotropic regions (56, 57).

10. A device as set forth in Claim 8, wherein the correcting means is installed in a place where the temperature and other environmental conditions are substantially the same as those for the torque detecting section.

11. A device as set forth in Claim 8,
wherein the exciting coil (16) for the first detecting coil (20) and the exciting coil (18) for the first correcting coil (22) being combined in series and connected to a first AC power source (27), and
wherein the exciting coil (17) for the second detecting coil (21) and the exciting coil (19) for the second correcting coil (23) being combined in series and connected to a second AC power source (26).

12. A device as set forth in Claim 11, including:
means (42, 41) for cutting off the outputs of the first and second power sources with suitable timing during torque measurement,
means for finding measured values provided by the first and second detecting coils (20, 21) and first and second correcting coils (22, 23) when said power sources (26, 27) are cut off, and

means for calibrating measured data by subtracting the readings in the two detecting coils (20, 21) and two correcting coils (22, 23) when said AC power sources (26, 27) are cut off from the measured values provided by said coils when the cut-off of said AC power sources is cancelled.

13. A device as set forth in Claim 12, including means for controlling one of the power sources (26, 27) so that the calibrated values of the measured data provided by the two correcting coils (22, 23) are equal.

14. A device as set forth in Claim 13, including means for controlling the two power sources (26, 27) so that the sum of the calibrated values of the measured data provided by the two detecting coils (20, 21) is a constant reference value.

15. A device as set forth in Claim 14, including means which, with constant timing, allows one of the following processes to be executed or two or more thereof to be serially executed:

the process for calibrating the measured data provided by the two detecting coils (20, 21),

the process for controlling one of the power sources (26, 27) so that the calibrated values of the measured data provided by the two correcting coils (22, 23) are equal, and
the process for controlling the two power sources (26, 27) so that the sum of the measured data provided by the two detecting coils (20, 21) is a constant reference value.

16. A device as set forth in Claim 15, including means (50, 51, 52) which makes it possible to execute at least one of said three processes to be executed manually at any time irrespectively of the constant timing.

17. A device for measuring torque acting on a shaft, comprising:

a torque detecting magnetically anisotropic region (12) formed on the outer peripheral surface of a torque transmitting shaft (11) and provided with magnetic anisotropy such that the region is inclined to form an angle with respect to the axis of rotation of said torque transmitting shaft (11),

a correcting magnetically anisotropic region (14) formed on the outer peripheral surface of the shaft (11) in the vicinity of the torque detecting magnetically anisotropic region (12) and provided with magnetic anisotropy in a direction parallel with the axis of

rotation of the shaft (11),

a detecting coil (20) and a correcting coil (22) installed along the peripheries of said torque detecting magnetically anisotropic region (12) and said correcting magnetically anisotropic region (14), respectively, including a detection-purpose exciting coil (16) associated with the detecting coil (20) and a correction-purpose exciting coil (17) associated with the correcting coil (22), and

means for controlling the exciting voltage applied to said exciting coil (17) of the correcting coil (22) to ensure that the measured data provided by said correcting coil (22) is equal to a constant reference value and for controlling the exciting voltage applied to said exciting coil (16) for said detecting coil (20) correspondingly to the control of said exciting voltage of the exciting coil (17) of said correcting coil (22).

18. A device as set forth in Claim 17, wherein said detection- and correction-purpose exciting coils (16, 17) are combined in series and connected to a power source (26).

19. A device as set forth in Claim 18, including:

means (42, 41) for cutting off the output of the power source (26) with suitable timing during torque measurement,

means for finding the measured data provided by the detecting and correcting coils (20, 22) when said power source output is cut off, and

means for calibrating data by subtracting the measured data provided by the detecting and correcting coils (20, 22) when said power source (26) is cut off from the measured data provided by said detecting and correcting coils (20, 22) when the cut-off of said power source (26) is cancelled.

20. A device as set forth in Claim 19, wherein the means for controlling the exciting voltage is constructed to effect control so that the calibrated value of the measured data provided by the correcting coil (22) is equal to the reference value.

21. A device as set forth in Claim 20, including means whereby the process for calibrating the measured data provided by the detecting and correcting coils (20, 22) and the process for controlling the power source (26) so that the calibrated value of the measured data provided by the correcting coil (22) are executed with constant timing.

22. A device as set forth in Claim 21, including means (50, 52) which makes it possible to execute one of the two processes to be executed manually at any time irrespectively of the constant timing.

Patentansprüche

1. Vorrichtung zur Messung eines auf eine Welle einwirkenden Drehmomentes, **gekennzeichnet durch:**

eine Drehmoment-Erfassungseinrichtung mit ersten und zweiten, magnetisch anisotropen Drehmoment-Erfassungsbereichen (12,13), die an einer äußeren peripheren Oberfläche einer Drehmoment-Übertragungswelle (11) ausgebildet und in der Weise mit einer magnetischen Anisotropie versehen sind, daß die Bereiche (12,13) zur Bildung von Winkeln in Bezug auf die Rotationsachse der Welle (11) in entgegengesetzte Richtungen geneigt sind, sowie mit ersten und zweiten Detektorspulen (20,21) zur Erfassung von Änderungen der Permeabilität in den magnetisch anisotropen Drehmoment-Erfassungsbereichen (12,13);

Erregerspulen (16,17,18,19), die für entsprechende Detektorspulen (20,21) und Korrekturspulen (22,23) vorgesehen sind; und

eine Korrektureinrichtung mit ersten und zweiten, magnetisch anisotropen Korrekturbereichen (14,15) mit einer in einer Richtung parallel zu der Rotationsachse der Welle (11) eingepprägten magnetischen Anisotropie, die auf der äußeren peripheren Oberfläche der Welle in der Nähe der ersten und zweiten, magnetisch anisotropen Drehmoment-Erfassungsbereiche (12,13) liegen; sowie mit ersten und zweiten Korrekturspulen (22,23) zur Erfassung von Änderungen der Permeabilität in den magnetisch anisotropen Korrekturbereichen (14,15).

2. Vorrichtung nach Anspruch 1, **dadurch gekennzeichnet,** daß die Erregerspule (16) für die erste Detektorspule (20) und die Erregerspule (18) für die erste Korrekturspule (22) in Serie geschaltet und mit einer ersten AC-Leistungsquelle (27) verbunden sind und daß die Erregerspule (17) für die zweite Detektorspule (21) und die Erregerspule (19) für die zweite Korrekturspule (23) in Serie geschaltet und mit einer zweiten AC-Leistungsquelle (26) verbunden sind.

3. Vorrichtung nach Anspruch 2, **gekennzeichnet durch:**

Einrichtungen (41,42) zum Abtrennen der Ausgänge der ersten und zweiten Leistungsquellen mit einer geeigneten Zeitsteuerung während

einer Drehmomentmessung;
 Einrichtungen zum Auffinden der gemessenen Werte, die durch die ersten und zweiten Detektorspulen (20,21) und die ersten und zweiten Korrekturspulen (22,23) erzeugt werden, wenn die Leistungsquellen abgetrennt sind; und
 Einrichtungen zur Kalibrierung von gemessenen Daten durch Subtraktion der gelesenen Werte in den zwei Detektorspulen und den zwei Korrekturspulen, wenn die AC-Leistungsquellen von den gemessenen Werten getrennt sind, die durch die Spulen erzeugt werden, wenn die Trennung der AC-Leistungsquellen aufgehoben ist.

4. Vorrichtung nach Anspruch 3, **gekennzeichnet durch** Einrichtungen zur Steuerung einer der AC-Leistungsquellen in der Weise, daß die kalibrierten Werte der gemessenen Daten, die durch die zwei Korrekturspulen (22,23) erzeugt werden, gleich sind.
5. Vorrichtung nach Anspruch 4, **gekennzeichnet durch** Einrichtung zur Steuerung der zwei AC-Leistungsquellen in der Weise, daß die Summe der kalibrierten Werte der gemessenen Daten, die durch die zwei Detektorspulen (20,21) erzeugt werden, einen konstanten Bezugswert darstellt.
6. Vorrichtung nach Anspruch 5, **gekennzeichnet durch** Einrichtungen, mit denen bei konstanter Zeitsteuerung einer der folgenden Vorgänge oder zwei oder mehrere dieser Vorgänge nacheinander ausgeführt werden können:
 der Vorgang der Kalibrierung der gemessenen Daten, die durch die zwei Detektorspulen (20,21) und die zwei Korrekturspulen (22,23) erzeugt werden,
 der Vorgang der Steuerung einer der Leistungsquellen (26,27) in der Weise, daß die kalibrierten Werte der durch die zwei Korrekturspulen erzeugten, gemessenen Daten gleich sind, und
 der Vorgang der Steuerung beider Leistungsquellen (26,27) gleichzeitig in der Weise, daß die Summe der kalibrierten Werte der durch die zwei Detektorspulen (20,21) erzeugten, gemessenen Daten einen konstanten Bezugswert darstellt.
7. Vorrichtung nach Anspruch 6, **gekennzeichnet durch** Einrichtungen (50,51,52) zur Ausführung mindestens eines der drei Vorgänge, die manuell zu jedem Zeitpunkt unabhängig von einer konstanten Zeitsteuerung ausgelöst werden.

8. Vorrichtung zur Messung eines auf eine Welle einwirkenden Drehmomentes, **gekennzeichnet durch**

eine Drehmoment-Erfassungseinrichtung mit ersten und zweiten, magnetisch anisotropen Drehmoment-Erfassungsbereichen (12,13), die an einer äußeren peripheren Oberfläche einer Drehmoment-Übertragungswelle (11) ausgebildet und in der Weise mit einer magnetischen Anisotropie versehen sind, daß die Bereiche (12,13) zur Bildung von Winkeln in Bezug auf die Rotationsachse der Welle (11) in entgegengesetzten Richtungen geneigt sind, sowie mit ersten und zweiten Detektorspulen (20,21) zur Erfassung von Änderungen der Permeabilität in den magnetisch anisotropen Drehmoment-Erfassungsbereichen (12,13);
 Erregerspulen (16,17,18,19), die für entsprechende Detektorspulen (20,21) und Korrekturspulen (22,23) vorgesehen sind; und
 eine Korrekturvorrichtung mit einer Korrekturwelle, die von der Drehmoment-Übertragungswelle (11) getrennt ist und keine Last aufweist und mit ersten und zweiten Korrekturspulen (22,23), die um die Korrekturwelle angeordnet sind, wobei
 die Korrekturvorrichtung im wesentlichen die gleichen magnetischen Eigenschaften wie die Drehmoment-Erfassungseinrichtung aufweist und in der Umgebung der Drehmoment-Erfassungseinrichtung angeordnet ist.

9. Vorrichtung nach Anspruch 8, **dadurch gekennzeichnet**, daß die
 Korrekturwelle erste und zweite, magnetisch anisotrope Korrekturbereiche (56,57) an ihrer äußeren peripheren Oberfläche aufweist, die zur Bildung von Winkeln in Bezug auf die Achse der Korrekturwelle in entgegengesetzte Richtungen geneigt sind, und daß
 die ersten und zweiten Korrekturspulen (22,23) entlang der Peripherie der ersten und zweiten, magnetisch anisotropen Bereiche (56,57) angeordnet sind.
10. Vorrichtung nach Anspruch 8, **dadurch gekennzeichnet**, daß die Korrekturvorrichtung an einer Stelle vorgesehen ist, an der die Temperatur- und andere Umgebungsbedingungen im wesentlichen die gleichen sind, wie an dem Drehmoment-Erfassungsteil.
11. Vorrichtung nach Anspruch 8, **dadurch gekennzeichnet**, daß die Erregerspule (16) für die erste Detektorspule (20) und die Erregerspule (18) für die erste Korrekturspule (22) in Serie geschaltet und mit einer ersten AC-Leistungsquelle (27) verbunden sind und

die Erregerspule (17) für die zweite Detektorspule (21) und die Erregerspule (19) für die zweite Korrekturspule (23) in Serie geschaltet und mit einer zweiten AC-Leistungsquelle (26) verbunden sind.

12. Vorrichtung nach Anspruch 11, gekennzeichnet durch:

Einrichtungen (41,42) zum Abtrennen der Ausgänge der ersten und zweiten Leistungsquellen in Abhängigkeit von einer geeigneten Zeitsteuerung während der Drehmomentmessung; Einrichtungen zum Auffinden der gemessenen Werte, die durch die erste und zweite Detektorspule (20,21) und die erste und zweite Korrekturspule (22,23) erzeugt werden, wenn die Leistungsquellen (26,27) abgetrennt sind; und Einrichtungen zum Kalibrieren der gemessenen Daten durch Subtraktion der aus den zwei Detektorspulen (20,21) und den zwei Korrekturspulen (22,23) gelesenen Werte, wenn die AC-Leistungsquellen (26,27) von den gemessenen Werten abgetrennt sind, die durch die Spulen erzeugt werden, wenn die Abtrennung der AC-Leistungsquellen aufgehoben ist.

13. Vorrichtung nach Anspruch 12, gekennzeichnet durch Einrichtungen zur Steuerung einer der Leistungsquellen (26,27) in der Weise, daß die kalibrierten Werte der durch die zwei Korrekturspulen (22,23) erzeugten, gemessenen Daten gleich sind.

14. Vorrichtung nach Anspruch 13, gekennzeichnet durch Einrichtungen zur Steuerung der zwei Leistungsquellen (26,27) in der Weise, daß die Summe der kalibrierten Werte der durch die zwei Detektorspulen (20,21) erzeugten, gemessenen Daten einen konstanten Bezugswert darstellt.

15. Vorrichtung nach Anspruch 14, gekennzeichnet durch Einrichtungen, mit denen bei konstanter Zeitsteuerung einer der folgenden Vorgänge oder zwei oder mehrere dieser Vorgänge seriell ausgeführt werden können: der Vorgang der Kalibrierung der durch die zwei Detektorspulen (20,21) erzeugten, gemessenen Daten,

der Vorgang der Steuerung einer der Leistungsquellen (26,27) in der Weise, daß die kalibrierten Werte der durch die zwei Korrekturspulen (22,23) erzeugten, gemessenen Daten gleich sind, und

der Vorgang der Steuerung der zwei Leistungsquellen (26,27) in der Weise, daß die Summe der gemessenen Daten, die durch die zwei Detektorspulen (20,21) erzeugt werden,

einen konstanten Bezugswert darstellt.

16. Vorrichtung nach Anspruch 15, gekennzeichnet durch

Einrichtungen (50,51,52), mit denen mindestens einer der drei manuell auszuführenden Vorgänge zu jedem Zeitpunkt unabhängig von einer konstanten Zeitsteuerung ausgeführt werden kann.

17. Vorrichtung zur Messung eines auf eine Welle einwirkenden Drehmomentes, gekennzeichnet durch:

einen magnetisch anisotropen Drehmoment-Erfassungsbereich (12), der an einer äußeren peripheren Oberfläche einer Drehmoment-Übertragungsquelle (11) ausgebildet und mit einer magnetischen Anisotropie in der Weise versehen ist, daß der Bereich zur Bildung eines Winkels in Bezug auf die Rotationsachse der Drehmoment-Übertragungswelle (11) schräg liegt; einen magnetisch anisotropen Korrekturbereich (14), der an einer äußeren peripheren Oberfläche der Welle (11) in der Umgebung des magnetisch anisotropen Drehmoment-Erfassungsbereichs (12) ausgebildet und mit einer magnetischen Anisotropie in einer parallel zu der Rotationsachse der Welle (11) verlaufenden Richtung versehen ist;

eine Detektorspule (20) und eine Korrekturspule (22), die entlang der Umfänge des magnetisch anisotropen Drehmoment-Erfassungsbereichs (12) bzw. des magnetisch anisotropen Korrekturbereichs (14) angeordnet sind, mit einer zur Detektion vorgesehenen Erregerspule (16), die der Detektorspule (20) zugeordnet ist und einer zur Korrektur vorgesehenen Erregerspule (17), die der Korrekturspule (22) zugeordnet ist; und

Einrichtung zur Steuerung der an die Erregerspule (17) der Korrekturspule (22) angelegten Erregerspannung, so daß die durch die Korrekturspule (22) erzeugten gemessenen Daten gleich einem konstanten Bezugswert sind, sowie zur Steuerung der Erregerspannung, die an die Erregerspule (16) für die Detektorspule (20) angelegt wird, entsprechend der Steuerung der Erregerspannung der Erregerspule (17) der Korrekturspule (22).

18. Vorrichtung nach Anspruch 17, dadurch gekennzeichnet, daß die zur Detektion und Korrektur vorgesehenen Erregerspulen (16,17) in Serie geschaltet und mit einer Leistungsquelle (26) verbunden sind.

19. Vorrichtung nach Anspruch 18, gekennzeichnet durch

Einrichtungen (42,41) zum Abtrennen des Ausgangs der Leistungsquelle (26) mit einer geeigneten Zeitsteuerung während der Drehmomentmessung, Einrichtungen zum Auffinden der durch die Detektor- und Korrekturspulen (20,22) erzeugten, gemessenen Daten, wenn der Ausgang der Leistungsquelle abgetrennt ist; und

Einrichtungen zur Kalibrierung von Daten durch Subtraktion der gemessenen Daten, die durch die Detektor- und Korrekturspulen (20,22) erzeugt werden, wenn die Leistungsquelle (26) von den durch die Detektor- und Korrekturspulen (20,22) erzeugten, gemessenen Daten abgetrennt ist, wenn die Abtrennung der Leistungsquelle (26) aufgehoben ist.

20. Vorrichtung nach Anspruch 19, **dadurch gekennzeichnet**, daß die Einrichtung zur Steuerung der Erregerspannung die Steuerung in der Weise bewirkt, daß der kalibrierte Wert der durch die Korrekturspule (22) erzeugten, gemessenen Daten gleich dem Bezugswert ist.

21. Vorrichtung nach Anspruch 20, **gekennzeichnet durch** Einrichtung, durch die der Vorgang der Kalibrierung der durch die Detektor- und Korrekturspulen (20,22) erzeugten, gemessenen Daten, sowie der Vorgang der Steuerung der Leistungsquelle (26) in der Weise, daß der kalibrierte Wert der durch die Korrekturspule (22) erzeugten, gemessenen Daten mit einem konstanten Zeittakt, ausgeführt wird.

22. Vorrichtung nach Anspruch 21, **gekennzeichnet durch**

Einrichtungen (50,52), mit denen einer der zwei manuell auszuführenden Vorgänge zu jedem Zeitpunkt unabhängig von dem konstanten Zeittakt ausgeführt werden kann.

Revendications

1. Dispositif de mesure d'un couple agissant sur un arbre, comprenant :
des moyens de détection de couple comportant une première zone et une seconde zone anisotropes de détection magnétique de couple (12, 13) formées sur la surface périphérique extérieure d'un arbre (11) et présentant une anisotropie magnétique telle que les zones (12, 13) soient inclinées dans des directions opposées pour former des angles par rapport à l'axe de rotation de l'arbre (11), et une première bobine et une seconde bobine de détection de couple (20, 21) capables de détecter des variations de perméabilité dans les zones de détection de couple magnétique-

ment anisotropes (12, 13), et des bobines d'excitation (16, 17, 18, 19) prévues pour les bobines de détection respectives (20, 21), et des bobines de correction (22, 23), et des moyens de correction comportant une première zone et une seconde zone de correction magnétiquement anisotropes (14, 15) auxquelles l'anisotropie magnétique est communiquée dans une direction parallèle à l'axe de rotation de l'arbre (11), ces zones étant formées sur la surface périphérique extérieure de l'arbre au voisinage de la première zone et de la seconde zone de détection de couple magnétiquement anisotropes (12, 13), tandis que la première bobine et la seconde bobine de correction (22, 23) sont capables de détecter des variations de perméabilité dans les zones de correction magnétiquement anisotropes (14, 15).

2. Dispositif selon la revendication 1, caractérisé en ce que la bobine d'excitation (16) de la première bobine de détection (20) et la bobine d'excitation (18) de la première bobine de correction (22) sont associées en série et branchées à une première source de courant alternatif (27), et en ce que la bobine d'excitation (17) de la seconde bobine de détection (21) et la bobine d'excitation (19) de la seconde bobine de correction (23) sont associées en série et branchées à une seconde source de courant alternatif (26).
3. Dispositif selon la revendication 2, caractérisé en ce qu'il comprend :
des moyens (41, 42) pour couper les sorties de la première source de courant et de la seconde source de courant suivant un minutage convenable pendant la mesure de couple,
des moyens pour trouver les valeurs mesurées fournies par la première bobine et la seconde bobine de détection (20, 21) et par la première bobine et la seconde bobine de correction (22, 23) lorsque les sources de courant sont coupées, et
des moyens pour étalonner les données mesurées en soustrayant les lectures des deux bobines de détection et des deux bobines de correction lorsque les sources de courant alternatif sont coupées, des valeurs mesurées fournies par ces bobines lorsqu'on supprime la coupure des sources de courant alternatif.
4. Dispositif selon la revendication 3, caractérisé en ce qu'il comprend des moyens pour commander l'une des sources de courant alternatif de façon que les valeurs étalonnées des valeurs mesurées fournies par les deux bobines

de correction (22, 23), soient égales.

5. Dispositif selon la revendication 4, caractérisé en ce qu'il comprend des moyens pour commander les deux sources de courant alternatif de façon que la somme des valeurs étalonnées des données mesurées fournies par les deux bobines de détection (20, 21), soit une valeur de référence constante.
6. Dispositif selon la revendication 5, caractérisé en ce qu'il comprend des moyens qui, avec un minutage constant, permettent d'effectuer l'une des opérations suivantes, ou d'effectuer en série deux ou plusieurs de ces opérations :
opération d'étalonnage des données mesurées fournies par les deux bobines de détection (20, 21) et les deux bobines de correction (22, 23),
opération de commande de l'une des sources de courant (26, 27) de façon que les valeurs étalonnées des données mesurées fournies par les deux bobines de correction, soient égales, et
opération de commande simultanée des deux sources de courant (26, 27) de façon que la somme des valeurs étalonnées des données mesurées fournies par les deux bobines de détection (20, 21), soit une valeur de référence constante.
7. Dispositif selon la revendication 6, caractérisé en ce qu'il comprend des moyens (50, 51, 52) permettant d'effectuer au moins l'une des trois opérations à effectuer manuellement à un moment quelconque, indépendamment du minutage constant.
8. Dispositif de mesure d'un couple agissant sur un arbre, caractérisé en ce qu'il comprend :
des moyens de détection de couple comportant une première zone et une seconde zone de détection de couple magnétiquement anisotropes (12, 13) formées sur la surface périphérique extérieure d'un arbre de transmission de couple (11) et présentant une anisotropie magnétique telle que les zones (12, 13) soient inclinées dans des directions opposées pour former des angles par rapport à l'axe de rotation de l'arbre (11, et
une première bobine et une seconde bobine de détection (20, 21) capables de détecter des variations de perméabilité dans les zones de détection de couple magnétiquement anisotropes (12, 13), et
des bobines d'excitation (16, 17, 18, 19) prévues respectivement pour les bobines de détection (20, 21) et les bobines de correction (22, 23), et

des moyens de correction comportant un arbre de correction séparé de l'arbre de transmission (11) et libre de charge, et

une première bobine et une seconde bobine de correction (22, 23) montées autour de l'arbre de correction, de sorte que les moyens de correction présentent essentiellement les mêmes propriétés magnétiques que les moyens de détection de couple, et sont montés au voisinage de ces moyens de détection de couple.

9. Dispositif selon la revendication 8, caractérisé en ce que :

l'arbre de correction comporte une première zone et une seconde zone de correction magnétiquement anisotropes (56, 57) sur sa surface périphérique extérieure, ces zones étant inclinées dans des directions opposées pour former des angles par rapport à l'axe de l'arbre de correction, et en ce que la première bobine et la seconde bobine de correction (22, 23) sont montées le long du pourtour de la première zone et de la seconde zone magnétiquement anisotropes (56, 57).

10. Dispositif selon la revendication 8, caractérisé en ce que les moyens de correction sont montés en un endroit où la température et les autres conditions d'environnement sont essentiellement les mêmes que celles de la partie de détection de couple.

11. Dispositif selon la revendication 8, caractérisé en ce que la bobine d'excitation (16) de la première bobine de détection (20) et la bobine d'excitation (18) de la première bobine de correction (22) sont associées en série et branchées à une première source de courant alternatif (27), et en ce que la bobine d'excitation (17) de la seconde bobine de détection (21) et la bobine d'excitation (19) de la seconde bobine de correction (23) sont associées en série et branchées à une seconde source de courant alternatif (26).

12. Dispositif selon la revendication 11, caractérisé en ce qu'il comprend :
des moyens (42, 41) pour couper les sorties de la première source de courant et de la seconde source de courant avec un minutage convenable pendant la mesure de couple,
des moyens pour trouver les valeurs mesurées fournies par la première bobine et la seconde bobine de détection (20, 21) et par la première bobine et la seconde bobine de correction (22, 23) lorsque les sources de courant (26, 27) sont coupées, et

des moyens pour étalonner les données mesurées en soustrayant les lectures des deux bobines de détection (20, 21) et des deux bobines de correction (22, 23), lorsque sont coupées, des valeurs mesurées fournies par ces bobines lorsqu'on supprime la coupure des sources de courant alternatif.

13. Dispositif selon la revendication 12, caractérisé en ce qu'il comprend des moyens pour commander l'une des sources de courant (26, 27) de façon que les valeurs étalonnées des données mesurées fournies par les deux bobines de correction (22, 23) soient égales.
14. Dispositif selon la revendication 13, caractérisé en ce qu'il comprend des moyens pour commander les deux sources de courant (26, 27) de façon que la somme des valeurs étalonnées des données mesurées fournies par les deux bobines de détection (20, 21), soit une valeur de référence constante.
15. Dispositif selon la revendication 14, caractérisé en ce qu'il comprend des moyens qui, avec un minutage constant, permettent d'effectuer l'une des opérations ci-après ou permettent d'effectuer en série deux ou plusieurs de ces opérations :
opération d'étalonnage des données mesurées fournies par les deux bobines de détection (20, 21),
opération de commande de l'une des sources de courant (26, 27) de façon que les valeurs étalonnées des données mesurées fournies par les deux bobines de correction (22, 23) soient égales, et
opération de commande des deux sources de courant (26, 27) de façon que la somme des données mesurées fournies par les deux bobines de détection (20, 21) soit une valeur de référence constante.
16. Dispositif selon la revendication 15, caractérisé en ce qu'il comprend des moyens (50, 51, 52) permettant d'effectuer au moins l'une des trois opérations à effectuer manuellement à un moment quelconque, indépendamment du minutage constant.
17. Dispositif de mesure d'un couple agissant sur un arbre, caractérisé en ce qu'il comprend :
une zone de détection de couple magnétiquement anisotrope (12) formée sur la surface périphérique extérieure d'un arbre de transmission de couple (11) et présentant une anisotropie magnétique telle que cette zone soit inclinée pour former un angle par rapport à l'axe

de rotation de l'arbre de transmission de couple (11),

une zone de correction magnétiquement anisotrope (14) formée sur la surface périphérique extérieure de l'arbre (11) au voisinage de la zone de détection de couple magnétiquement anisotrope (12), et présentant une anisotropie magnétique dans une direction parallèle à l'axe de rotation de l'arbre (11),

une bobine de détection (20) et une bobine de correction (22) montées respectivement le long des pourtours de la zone de détection de couple magnétiquement anisotrope (12) et de la zone de correction magnétiquement anisotrope (14), comprenant une bobine d'excitation à but de détection (16) associée à la bobine de détection (20), et une bobine d'excitation à but de correction (17) associée à la bobine de correction (22), et

des moyens de commande de la tension d'excitation appliquée à la bobine d'excitation (17) de la bobine de correction (22) pour s'assurer que les données mesurées fournies par la bobine de correction (22) soient égales à une valeur de référence constante, et pour commander la tension d'excitation appliquée à la bobine d'excitation (16) de la bobine de détection (20) en correspondance avec la commande de la tension d'excitation de la bobine d'excitation (17) de la bobine de correction (22).

18. Dispositif selon la revendication 17, caractérisé en ce que la bobine d'excitation à but de détection (16) et la bobine d'excitation à but de correction (17) sont associées en série et branchées à une source de courant (26).

19. Dispositif selon la revendication 18, caractérisé en ce qu'il comprend des moyens (42, 41) pour couper la sortie de la source de courant (26) avec un minutage des moyens pour trouver les données mesurées fournies par la bobine de détection et la bobine de correction (20, 22) lorsque la sortie de la source de courant est coupée, et
des moyens pour étalonner les données en soustrayant les données mesurées fournies par la bobine de détection et la bobine de correction (20, 22) lorsque la source de courant (26) est coupée, des données mesurées fournies par la bobine de détection et la bobine de correction (20, 22) lorsqu'on supprime la coupure de la source de courant (26).

20. Dispositif selon la revendication 19, caractérisé en ce que les moyens de commande de la tension d'excitation sont réalisés pour effectuer la commande de façon que la valeur étalonnée

des données mesurées fournies par la bobine de correction (22), soit égale à la valeur de référence.

21. Dispositif selon la revendication 20, caractérisé en ce qu'il comprend des moyens permettant d'effectuer avec un minutage constant l'opération d'étalonnage des données mesurées fournies par la bobine de détection et la bobine de correction (20, 22), et l'opération de commande de la source de courant (26) de façon que la valeur étalonnée des données mesurées soit fournie par la bobine de correction (22). 5 10
22. Dispositif selon la revendication 21, caractérisé en ce qu'il comprend des moyens (50, 52) permettant d'effectuer l'une des deux opérations à effectuer manuellement, à un moment quelconque indépendamment du minutage constant. 15 20

25

30

35

40

45

50

55

60

FIG. 1

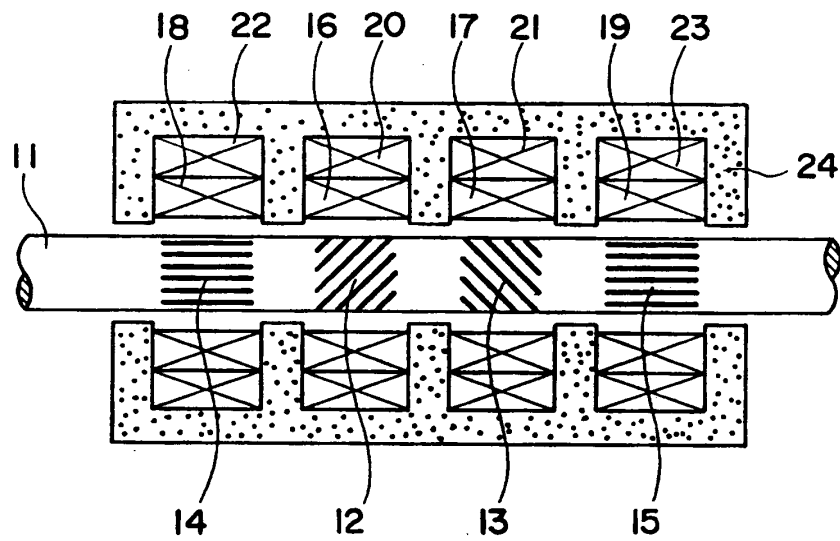


FIG. 2

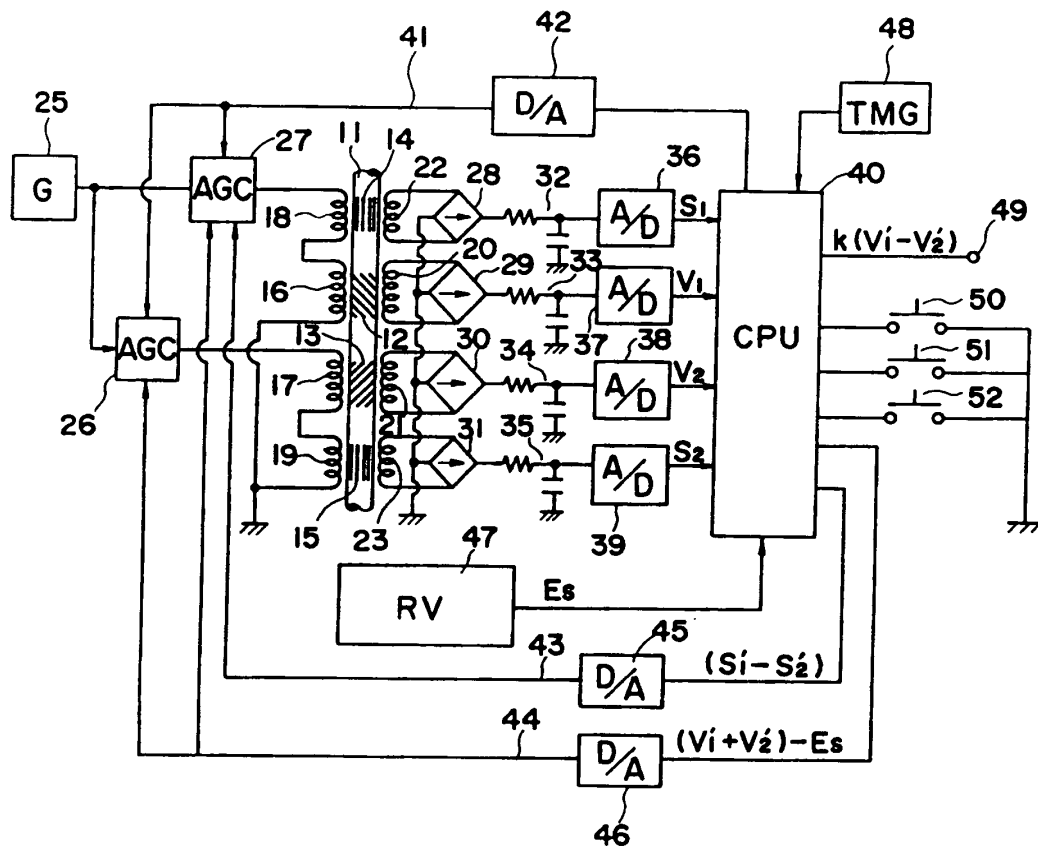


FIG. 3

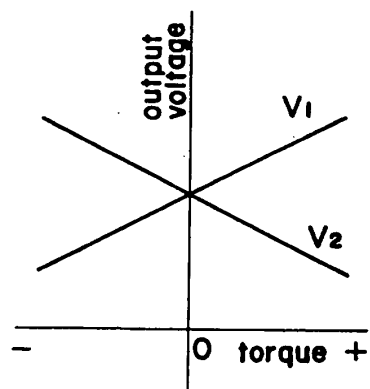


FIG. 5

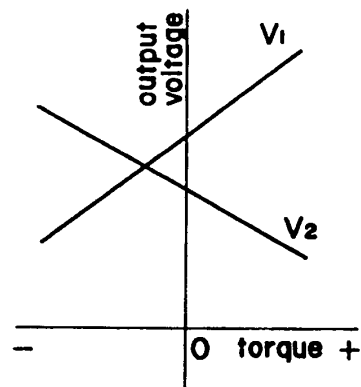
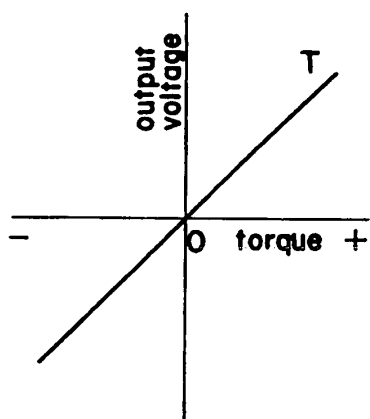
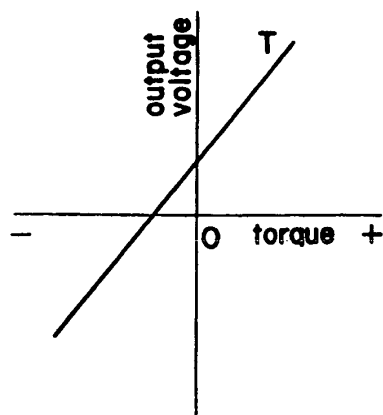


FIG. 4



$$T = k(V_1 - V_2)$$

FIG. 6



$$T = k(V_1 - V_2)$$

FIG. 7

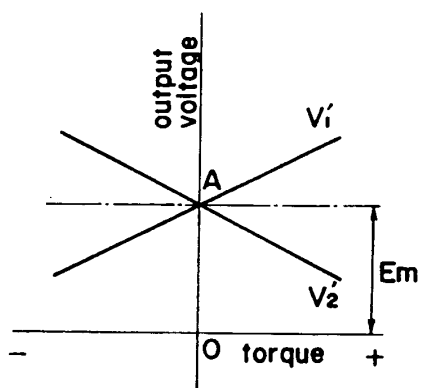


FIG. 8

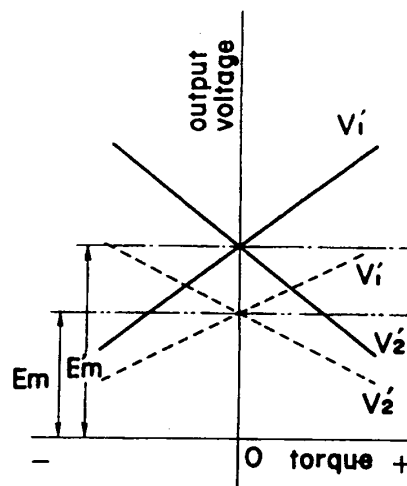


FIG. 9

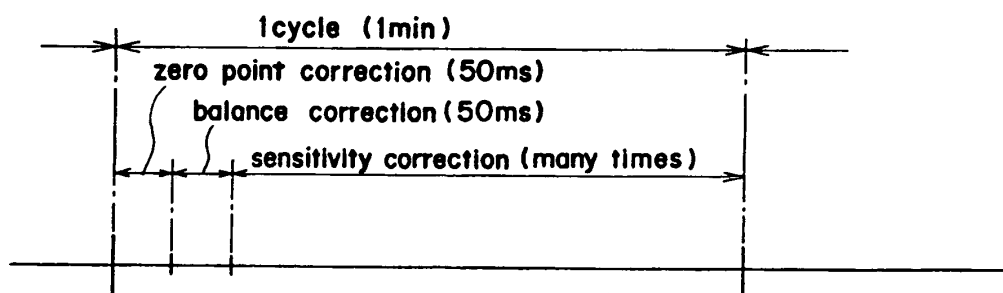


FIG. 10

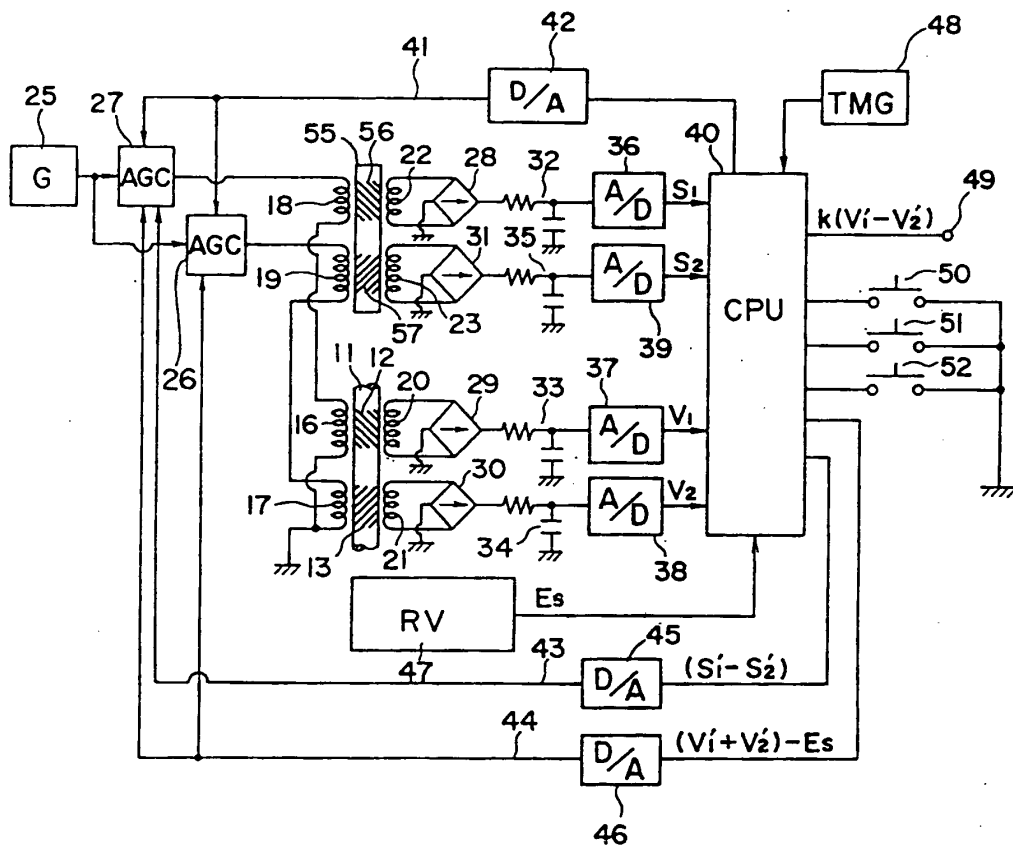


FIG. 11

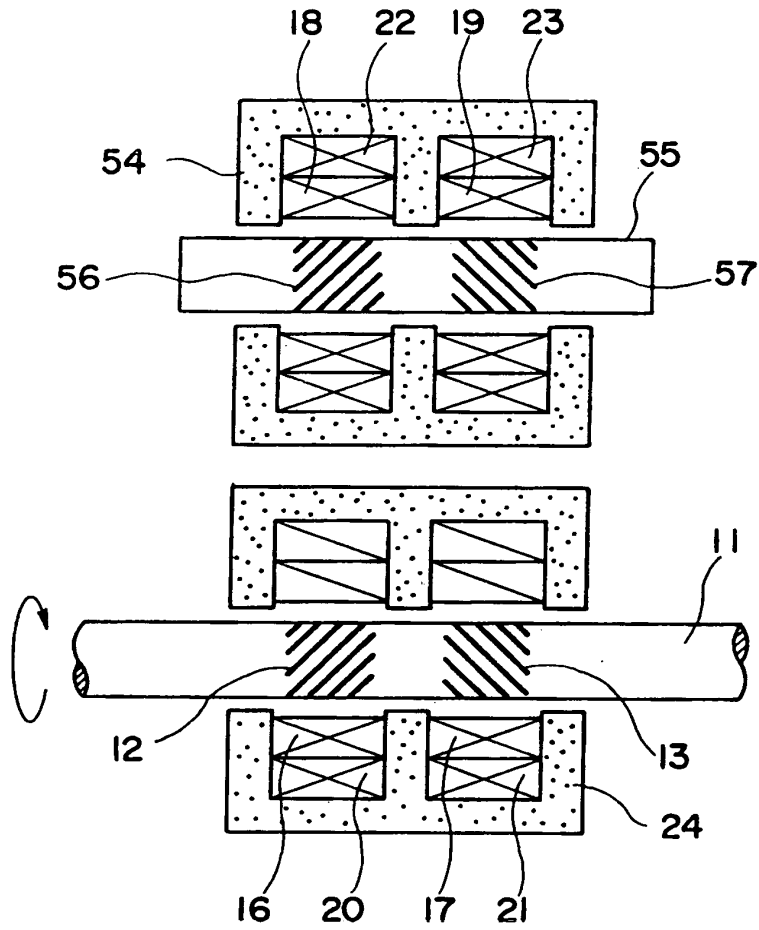


FIG. 12

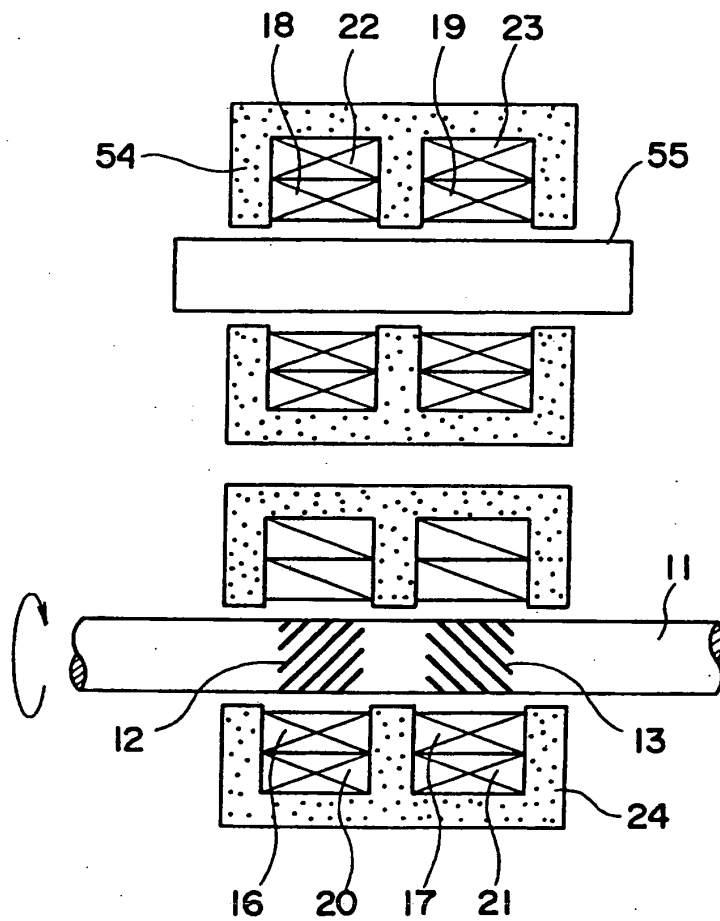


FIG. 13

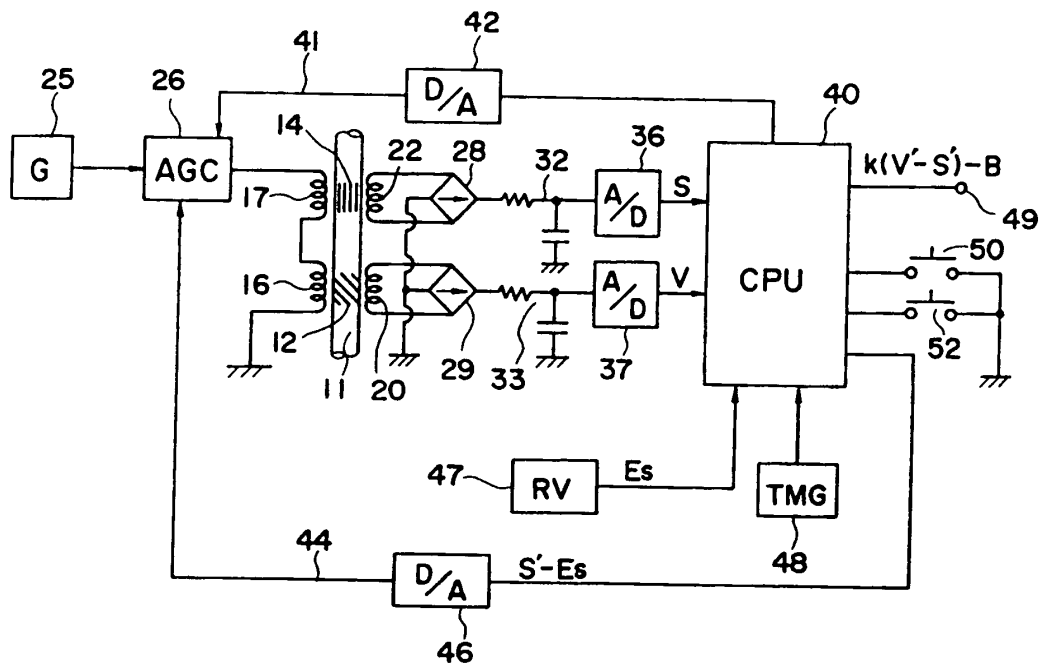


FIG. 14

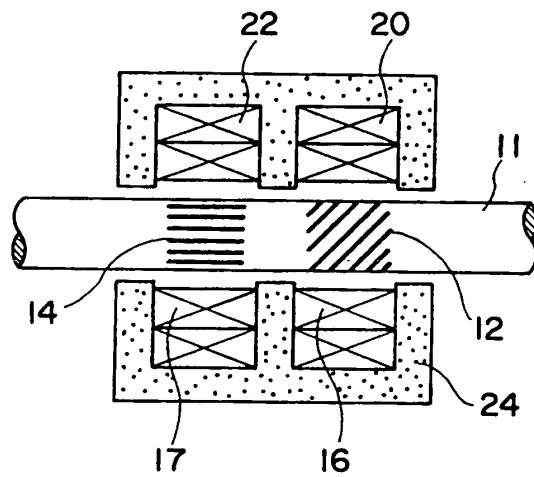


FIG. 15

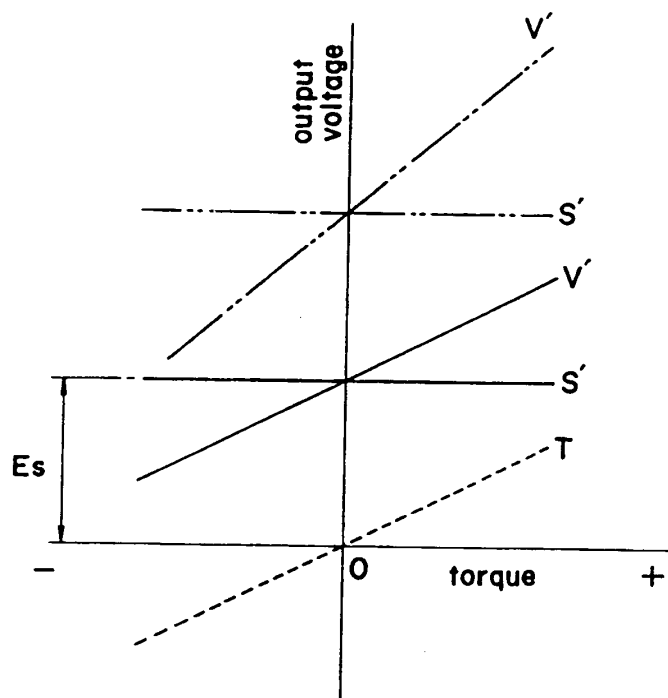


FIG. 16

